

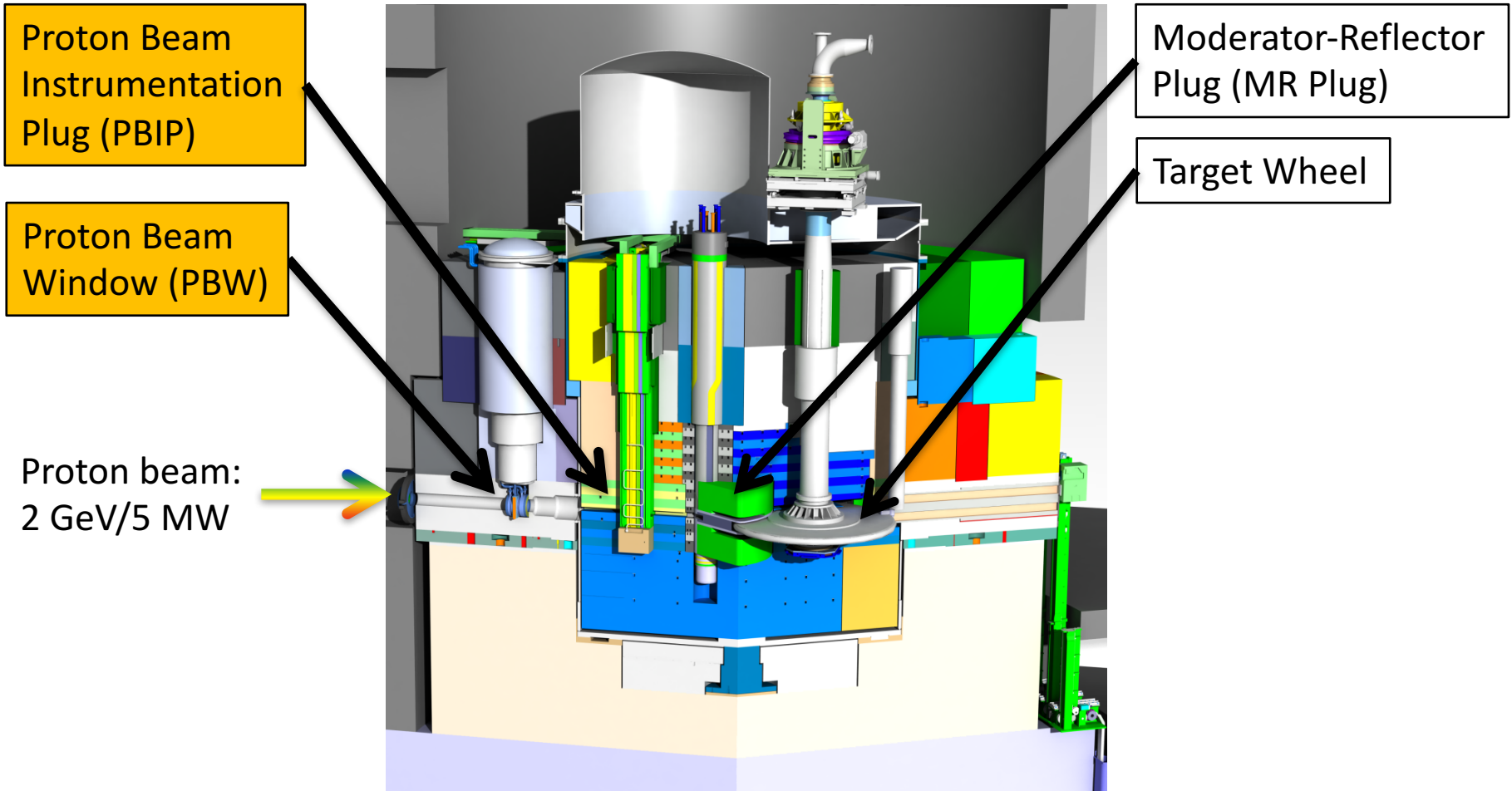
Material Selection of the Beam Profile Monitoring Devices at ESS Target Station

Y. Lee, M. Hartl, C. Thomas, T. Shea, J. Habainy

Need for beam profile monitoring (BPM)

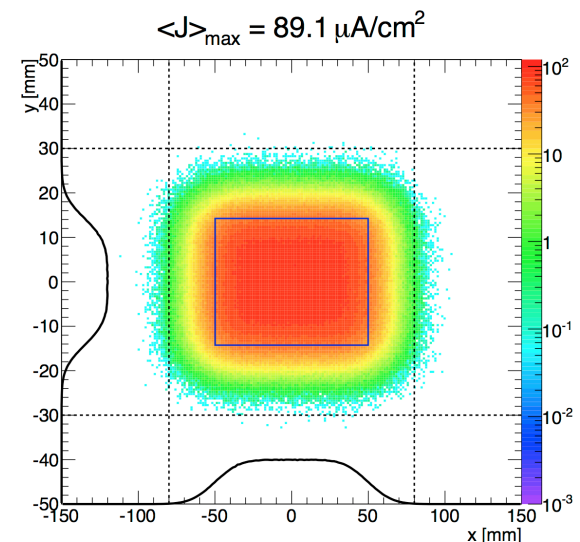
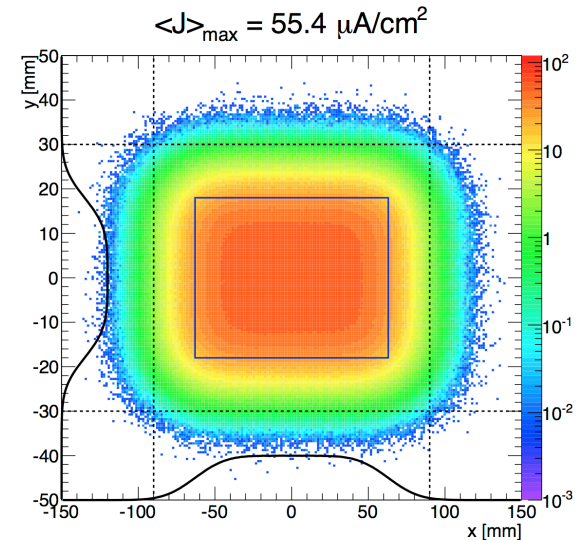
- ESS beam parameters
 - 2 GeV, 5 MW proton beam
 - 4% duty factor
 - 14 Hz repetition rate
 - Pulse duration of 2.86 ms
 - 2.5 mA (5 MW) time averaged beam current
 - 62.5 mA (125 MW) beam current during pulse
- BPM is required to avoid a target systems failure due to an anomalous beam.
 - Beam current density
 - Beam halo distribution
 - Beam position

Target Monolith – Beam Diagnostics



Design Beam Profile on Target

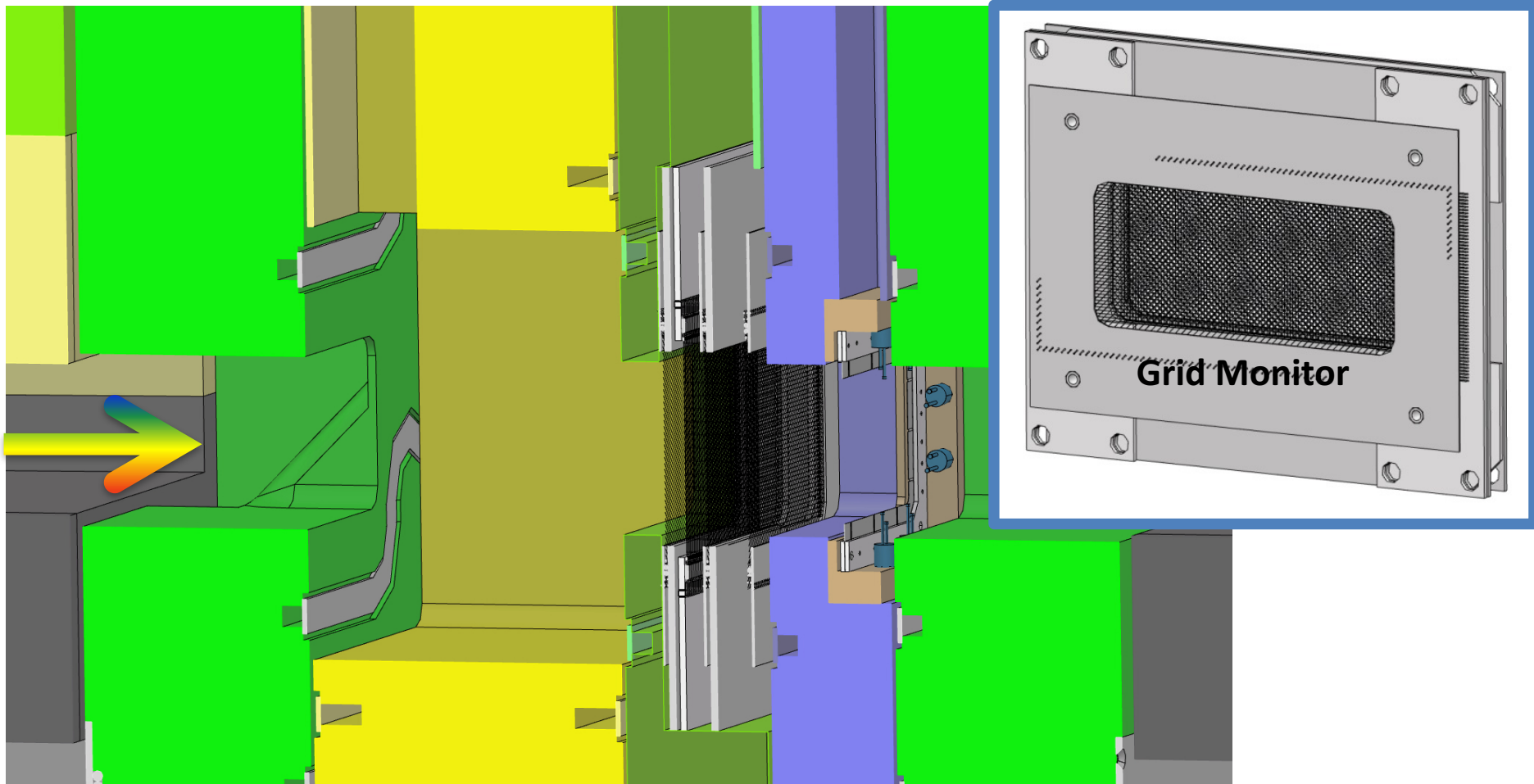
- Beam on target requirements:
 - Beam footprint enclosing 97.5% beam fraction: 180 mm (H) × 60 mm (V)
 - Beam footprint enclosing 99.9% beam fraction: 200 mm (H) × 64 mm (V)
 - Nominal time-averaged peak current density: $56 \mu\text{A}/\text{cm}^2$
 - Maximum time-averaged peak current density: $81 \mu\text{A}/\text{cm}^2$
 - Max displacement of footprint from nominal position: ± 5 mm (H), ± 3 mm (V)
- Beam on PBW:
 - Higher beam current density, assuming linear optics.



Beam Profile Monitoring System

- All the BPM systems planned is based on beam-intersecting
 - High irradiation damage induced short service lifetime
 - High thermal load induced structural failure
- Baseline scope of the BPM Systems at the Target Station:
 - Multi-wire profile monitor (MWPM):
 - Set of conducting wires intersecting proton beam
 - Aperture monitor:
 - Set of thin metal blades intersecting the proton beam edge
 - Luminescent coating:
 - Proton beam window (PBW)
 - Beam entrance window (BEW) of the target wheel

Proton Beam Instrumentation Plug

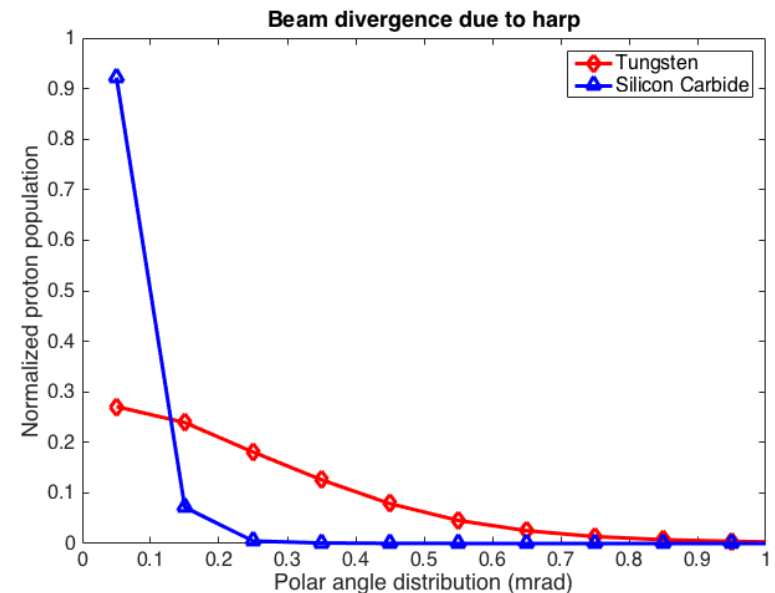


Material choice for harp

- Candidate Materials
 - Pure tungsten: SNS
 - Tungsten-Rhenium alloy: BLIP
 - SiC: JSNS, ISIS, LANSCE
- Material Selection Criteria
 - Disturbance to beam optics
 - Signal characteristics
 - Lifetime limited by radiation damage
 - Endurance to thermal and mechanical loads

Harp material: Disturbance to beam optics

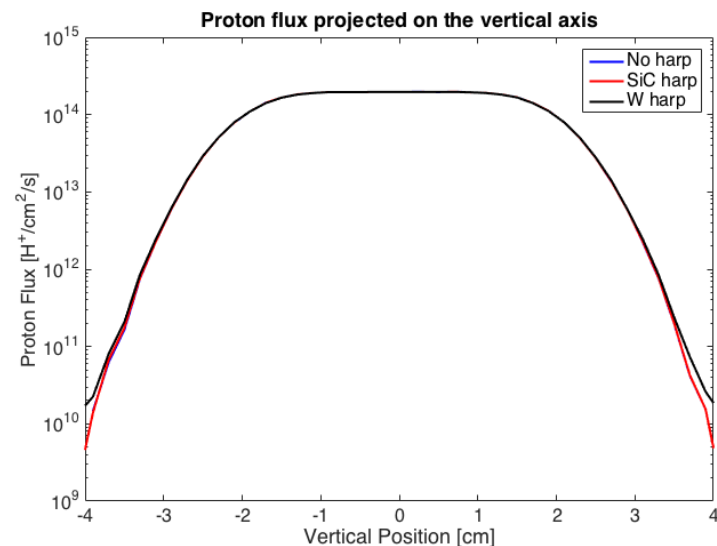
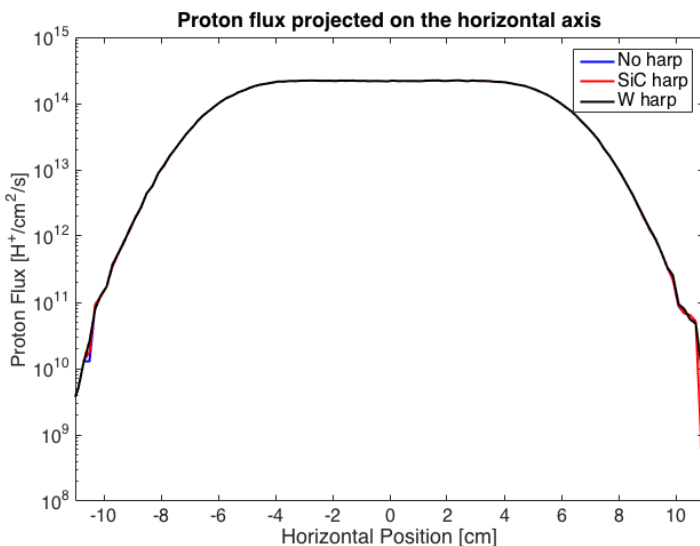
- There are five layers of harp made of 100 μm thick wires with a pitch of 2 mm.
- For a pencil beam, the beam diverges with:
 - SiC harp: 0.06 mrad
 - W harp: 0.25 mrad



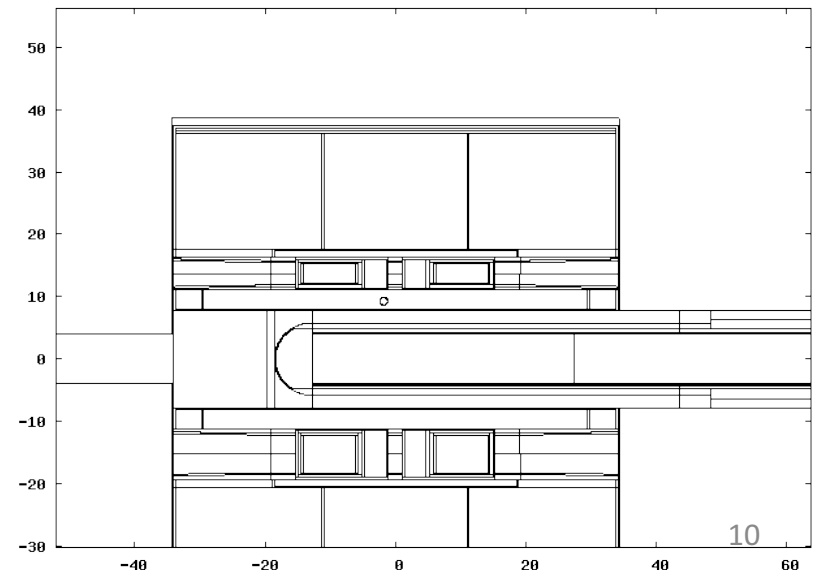
Effect of harps on beam-on-target requirement

Harp	Envelop 180 mm (H) × 60 mm (V)	Envelop 200 mm (H) × 64 mm (V)
No harp	99.38%	99.89%
SiC harps	99.37%	99.88%
W harps	99.33%	99.85%

- With the W harps, the beam shooting off the target is in an order of 1 kW compared to SiC harps.



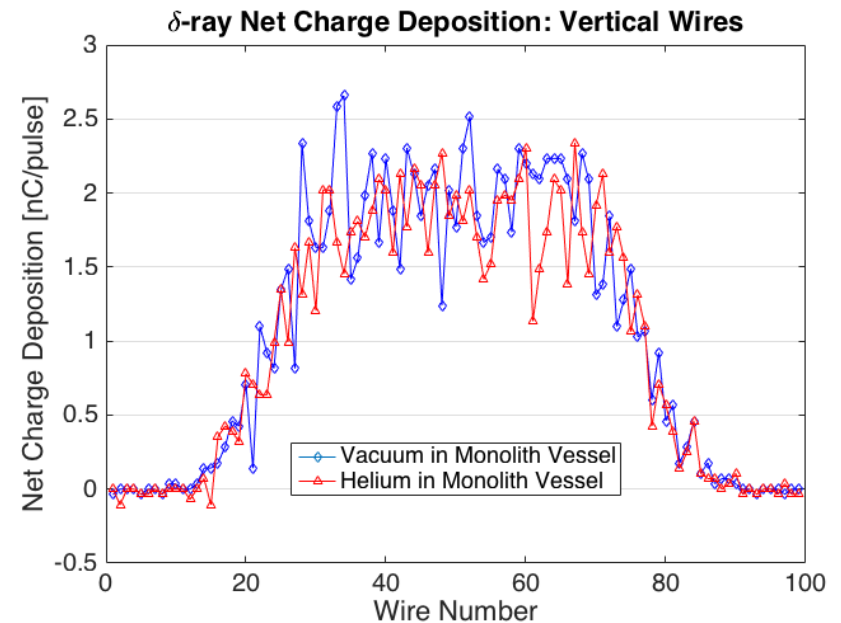
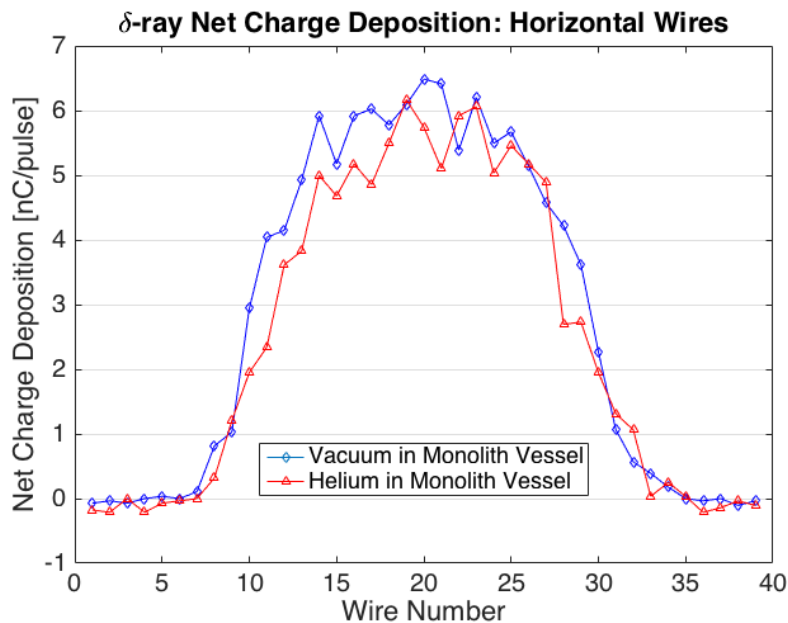
- Negative charge deficiency
 - Secondary electron emission (SEE)
 - Ionization, diffusion of slow secondaries to the surface, subsequent escape of electrons
 - Secondary electron yield (SEY) is calculated by an empirical formula:
$$SEY = \frac{P \cdot d_s}{E^*} \frac{dE}{dz}$$
 - Recoiled delta ray electrons
 - Directly calculated by FLUKA



Signal Strength

Harp Material	dE/dz [MeV/cm]@2GeV-H ⁺	Secondary electron yield	Delta ray electron yield	Total Yield	Benchmark
W	24.4	0.049	0.026	0.075	0.07 SNS: 1 GeV-H ⁺
SiC	5.16	0.010	0.013	0.023	0.01 LANSCE: 0.8 GeV-H ⁺

- The signal from the tungsten harp is more than three times higher.



Radiation Damage

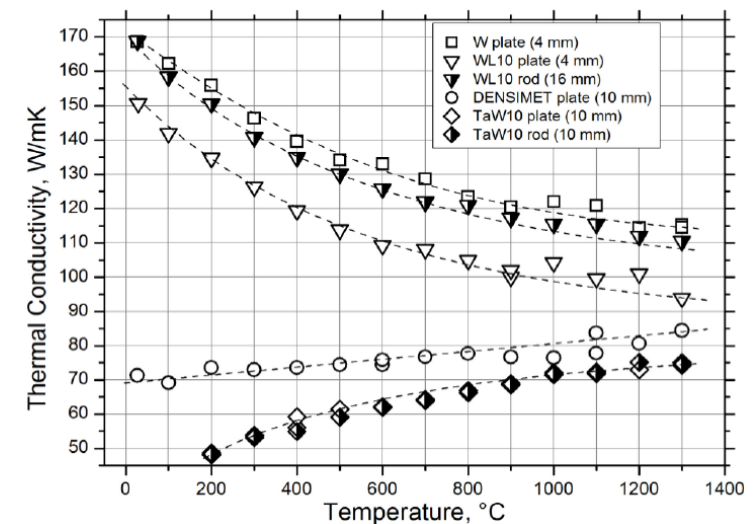
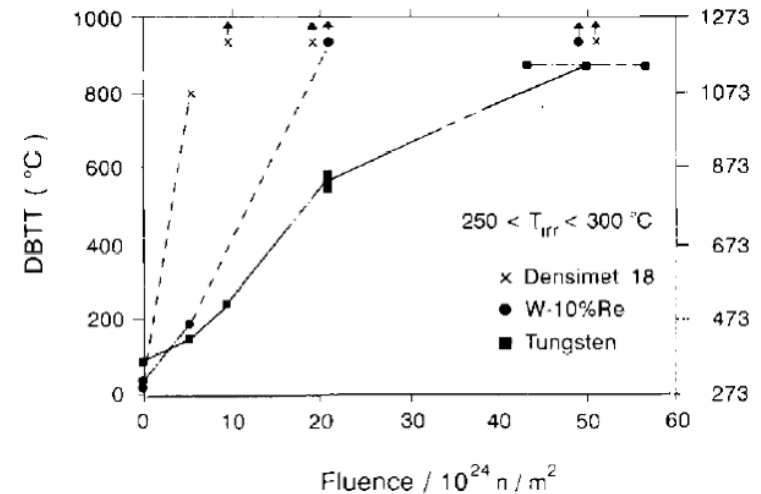
Harp Material	Max. DPA Rate [dpa/hour]	Annual Beam on Target Time	Max. DPA per Year
W	0.012	5400	64.8
SiC	0.001	5400	5.4

- The tungsten harp at SNS and the SiC harp at TS2 of ISIS have been operating without failure since its commissioning of the facilities.
- The accumulated damage dose on the harp in both facilities is roughly equivalent to one year dose at ESS.

Benchmarking Institution	Harp Material	Total Beam Energy/Charge	Accumulated Max. DPA
ORNL-SNS	W	32000 MWh	70
ISIS-TS2	SiC	1.5 Ah	3

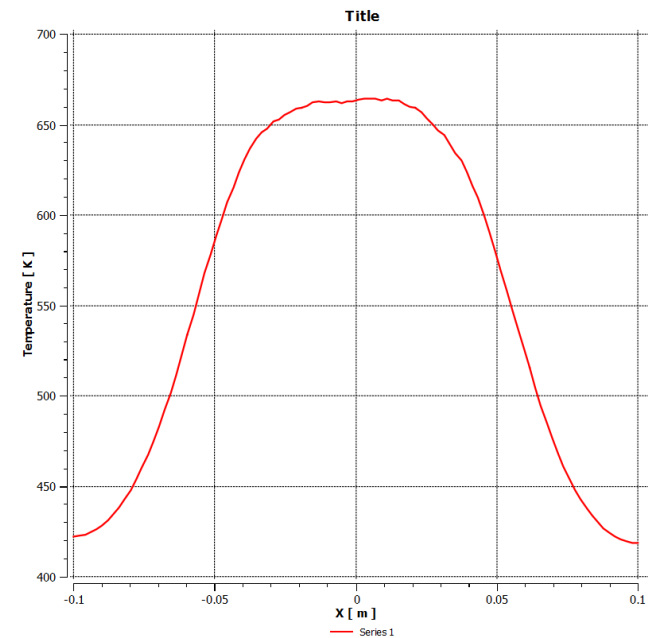
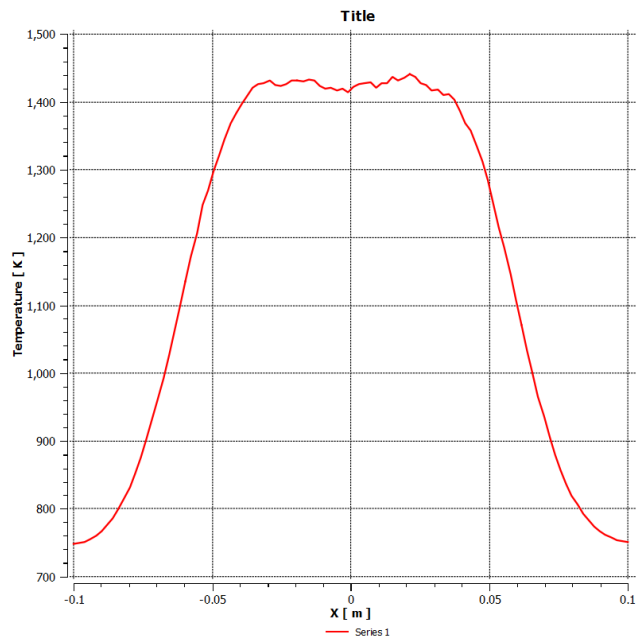
Early failure of W-Re Harp at BLIP

- The DBTT of W-Re alloy gets higher than pure tungsten after irradiation [H. Ullmaier, F. Carsughi, NIM-B 101, 1995]
- The thermal conductivity of W-Re alloy is lower than pure tungsten, which should lead to a higher thermo-mechanical stress and fatigue stress amplitude [M. Rieth et al, Tech- Rep.-KIT]



Thermal and mechanical properties

	Tungsten	SiC
Post-pulse maximum temperature	1420 K	660 K
Post-pulse maximum stress	77 MPa	76 MPa
Yield Stress/Flexural Strength	200 MPa	415 MPa

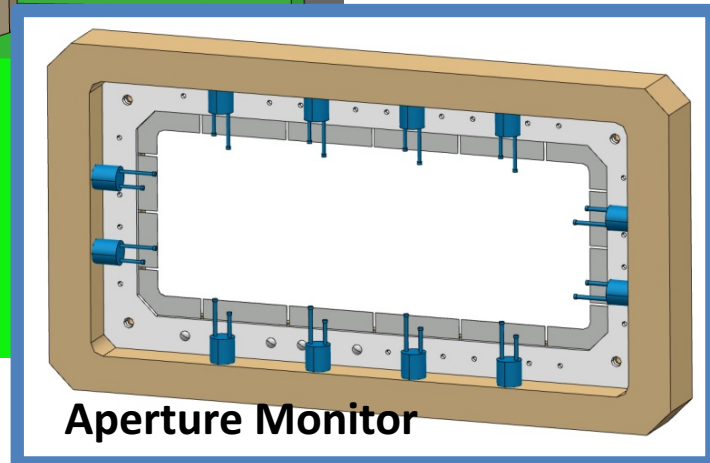
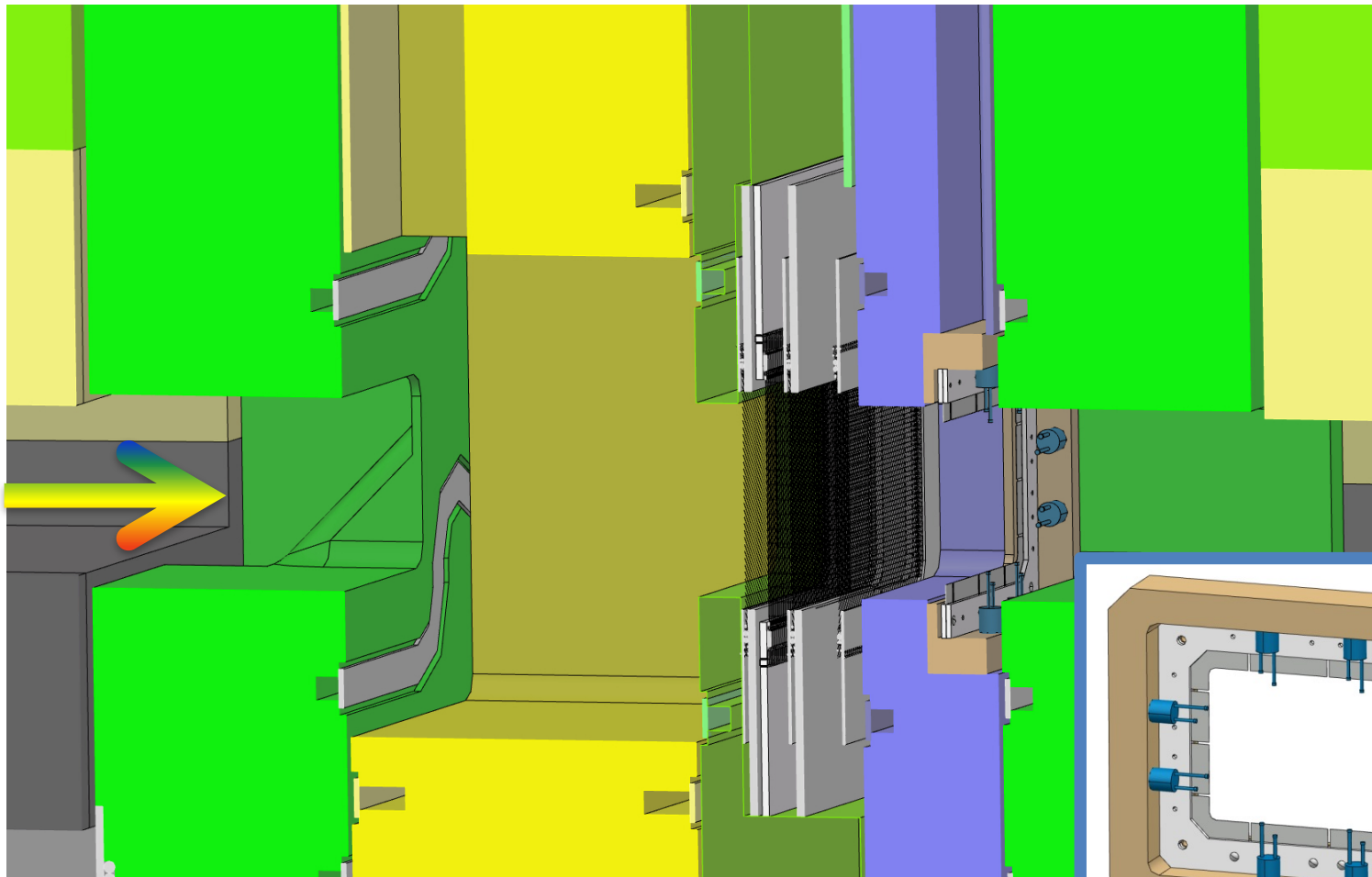


Tungsten vs. SiC

Properties	Tungsten	SiC
Beam optics disturbance	-	0
Δ -ray production	--	-
Radiation damage limit	1 year@5 MW	1 year@5 MW
Signal strength	+	-
Surface corrosion	-	+
Operation temperature	High	Medium
Mechanical load during operation	High	Low

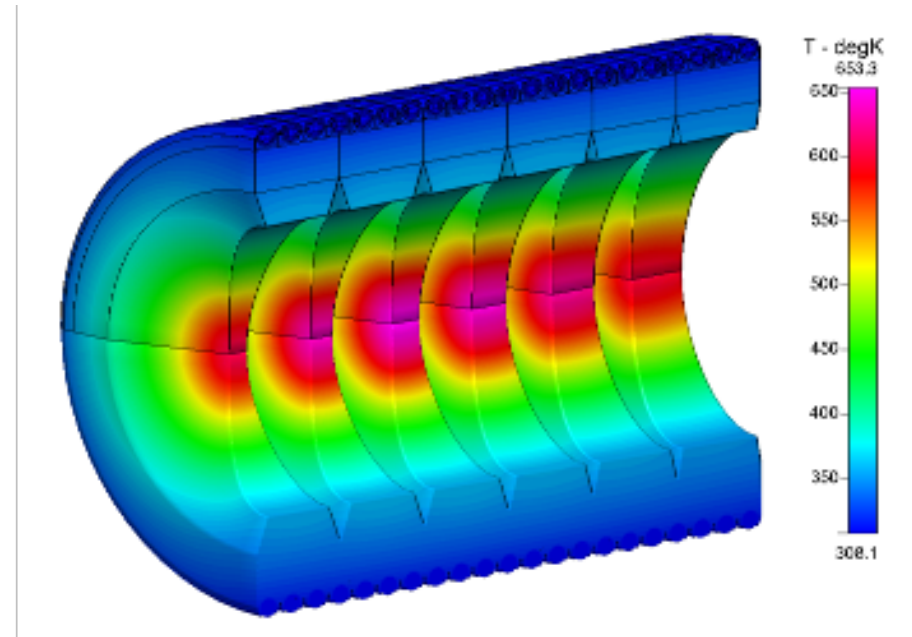
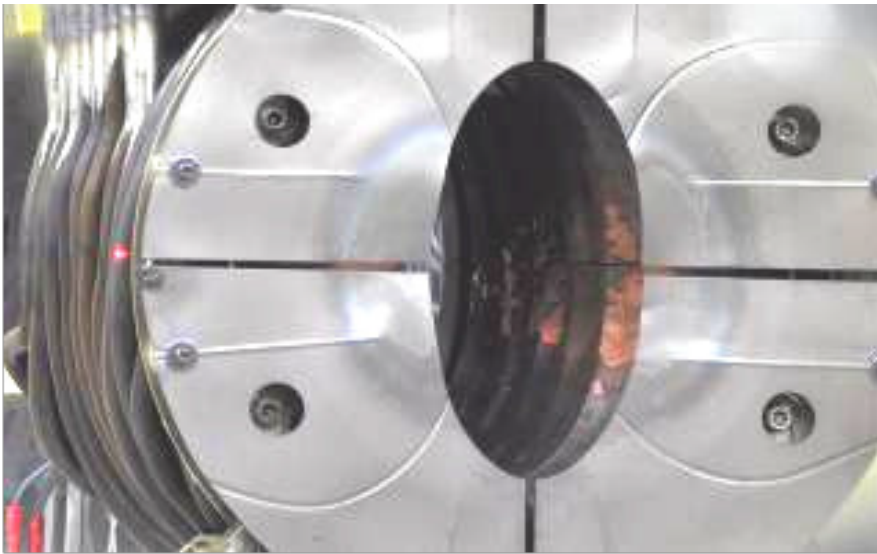
- Silicon Carbide is preferred for the ESS application

Proton Beam Instrumentation Plug



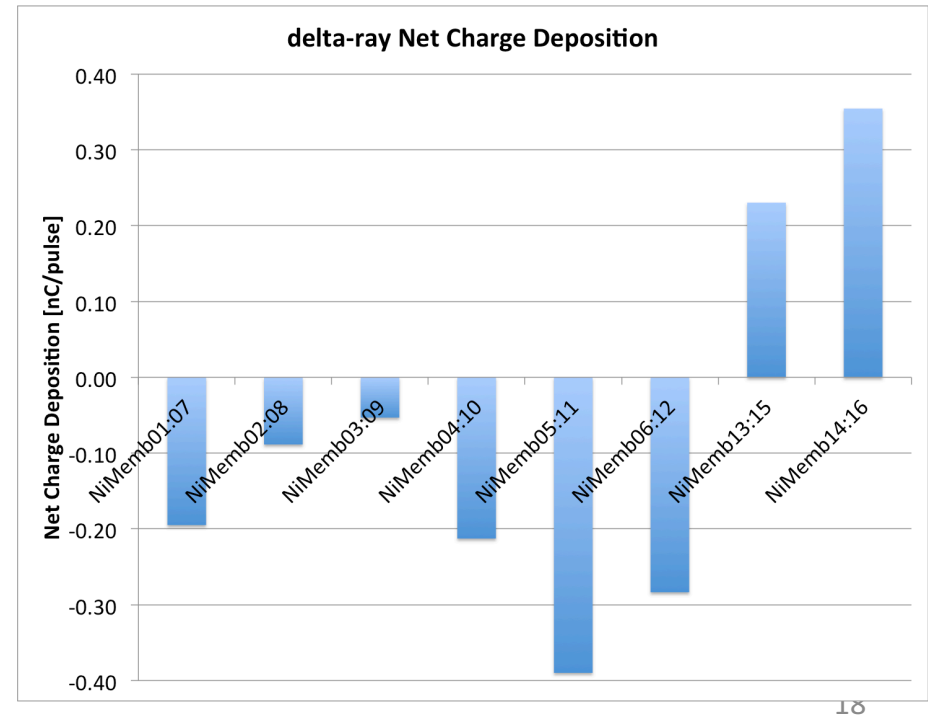
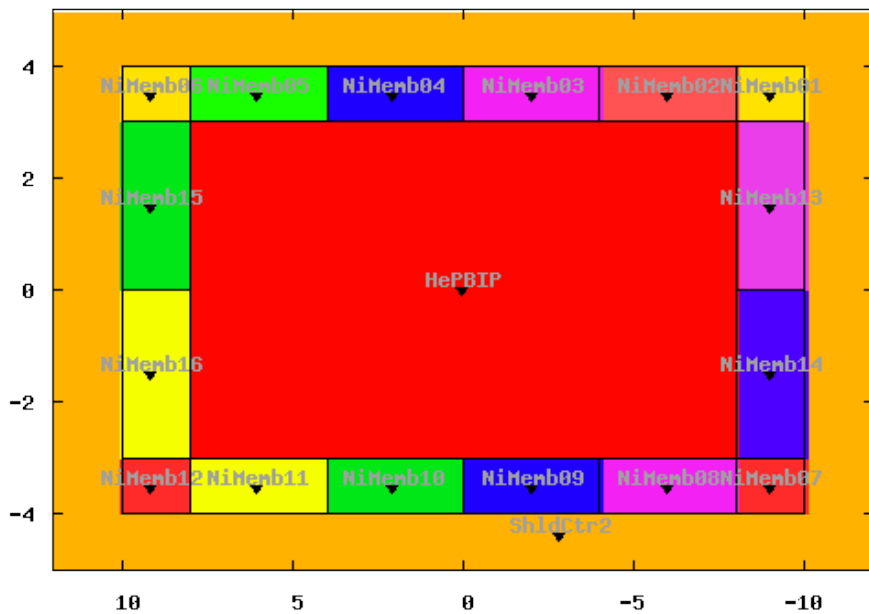
Aperture Monitor

- Material Selection: Nickel
 - The halo monitor mounted at the direct beam upstream of KHE-2 is made of 100 μm thick nickel membrane.



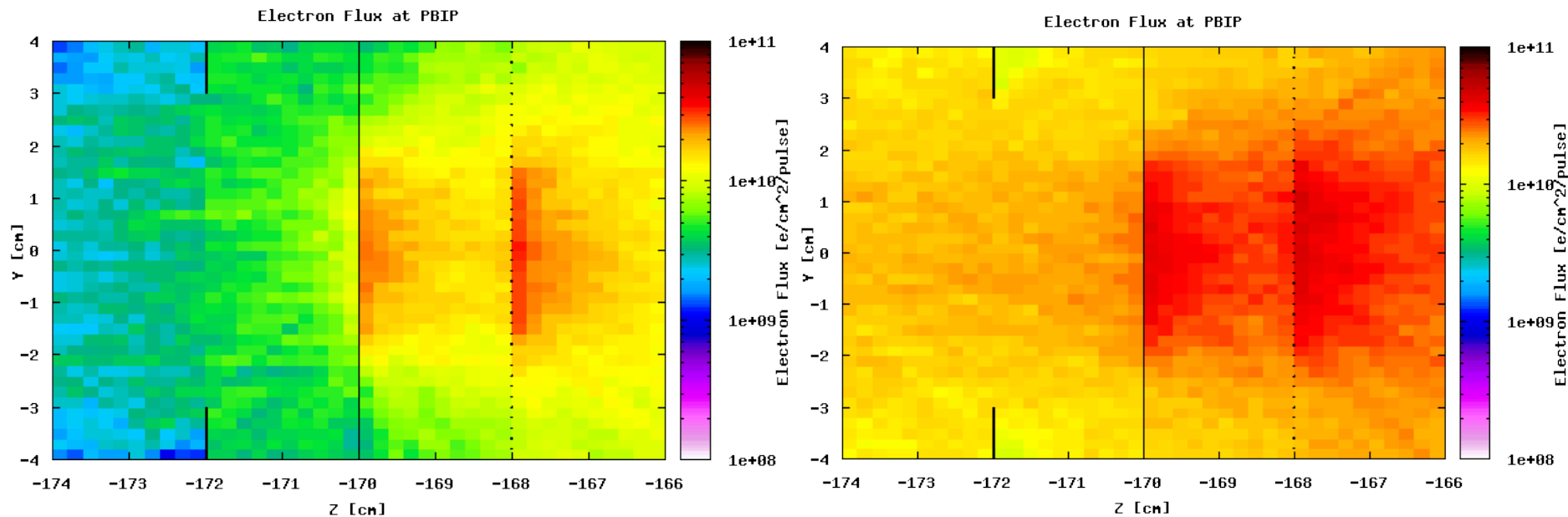
Signal Strength: 100 um thin Ni-Diaphragm

Facility	dE/dz [MeV/cm]	Secondary Electron Yield	δ -Ray Yield	Total Yield
PSI	16.7	0.033	0.023	0.056
ESS	13.6	0.027	0.019	0.046



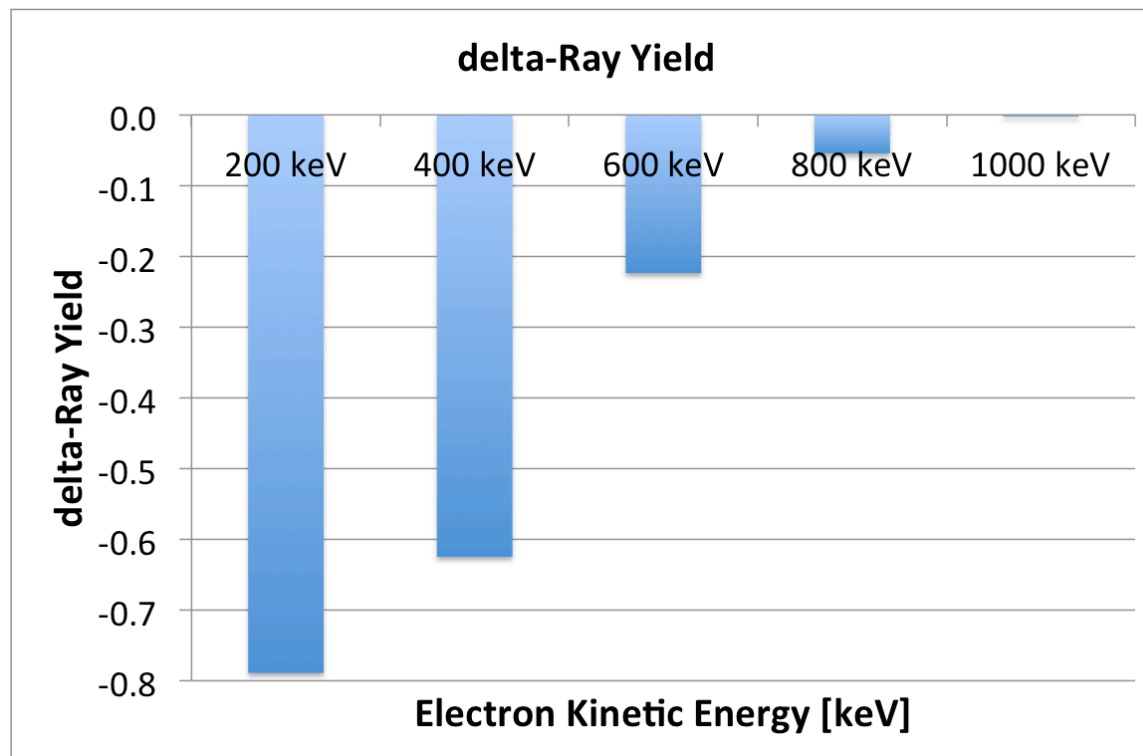
Negative Net-Charge Deposition

- Δ -rays from harp and helium atmosphere



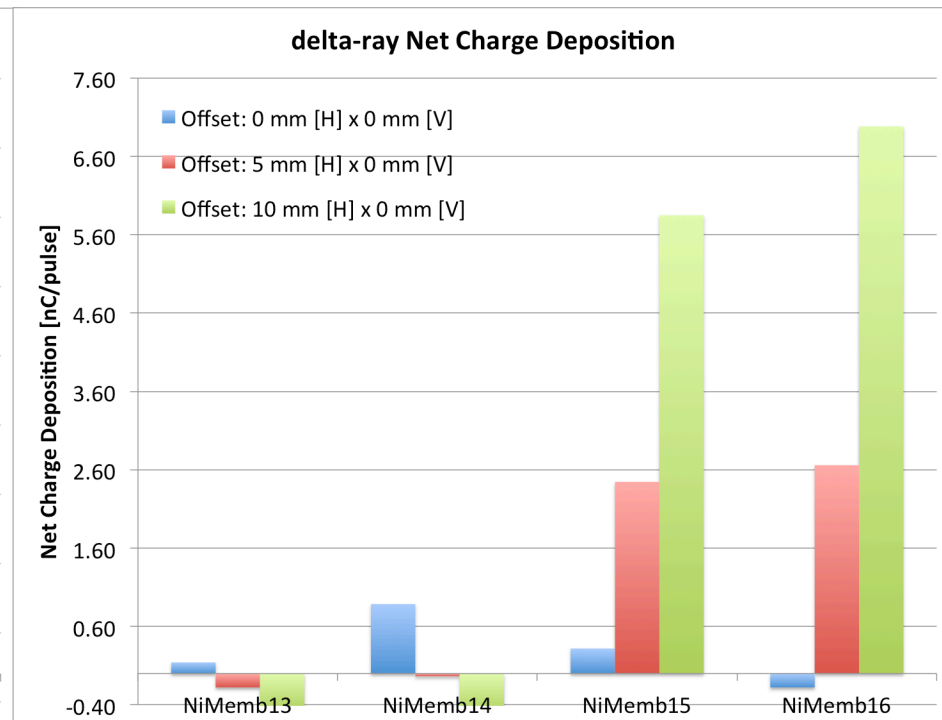
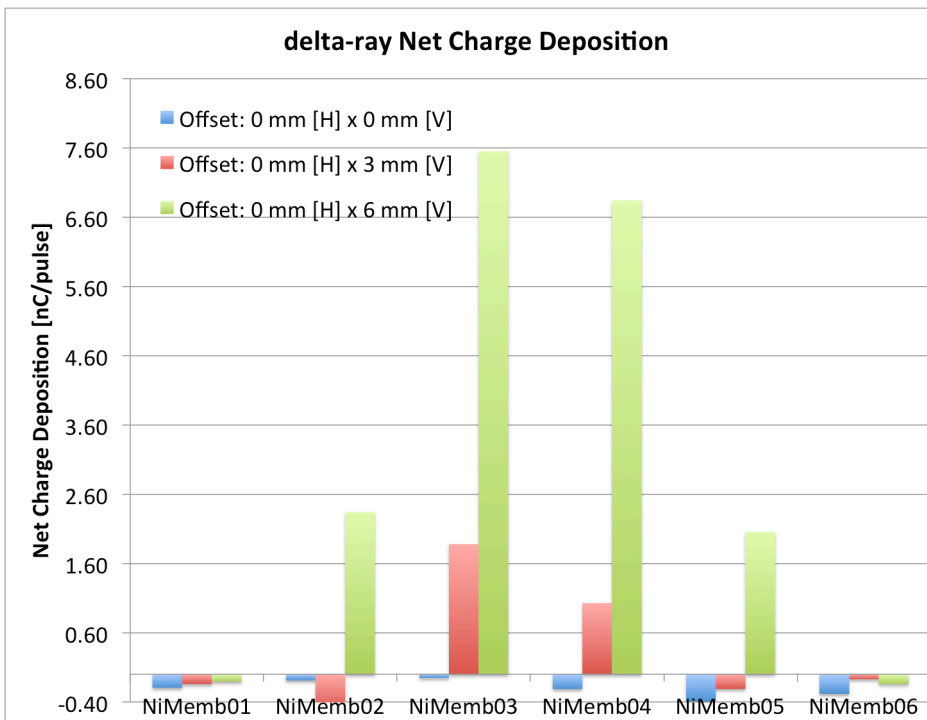
Δ -ray yield due to impinging δ -ray electrons

- The calculated δ -rays are in the energy range between 10 keV and 1 MeV
- Low energy δ -rays are stopped within the 100 μm thickness of the Ni-diaphragm, creating negative net charge deposition.



Beam offset and δ -ray yield

- As there are more protons bombarding the blade, the net charge yield turns to “positive”

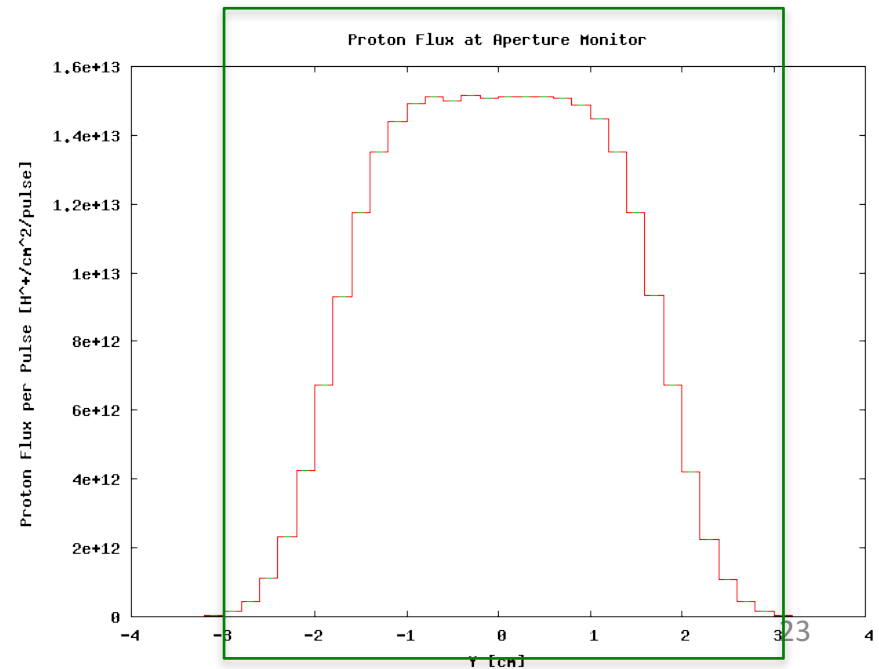
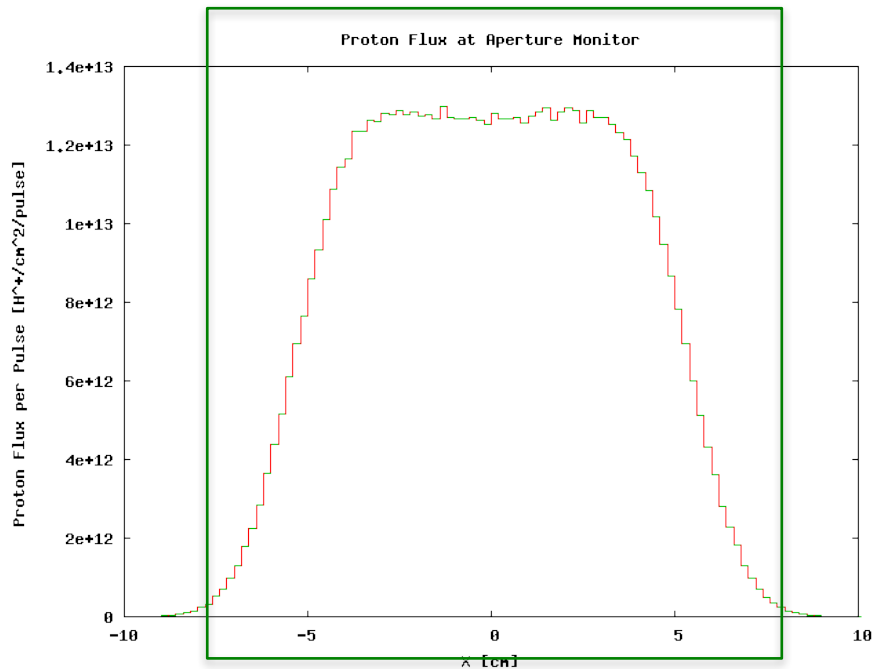


Radiation Damage and Lifetime

- Benchmarking: PSI
 - Integrated beam charge up to 2010: 120 Ah
 - Maximum integrated DPA: 100
- Aperture monitor at ESS
 - Maximum damage rate: < 10 dpa/year for 27000 MWh/y
 - The lifetime of the aperture monitor is conservatively estimated to be 10 years

Temperature at Aperture Monitor

- The maximum volumetric energy density per pulse is 1 J/cm³/pulse.
- The dynamic temperature amplitude per pulse is less than 1 °C.
 - A small beam offset will increase the maximum temperature amplitude per pulse rapidly.

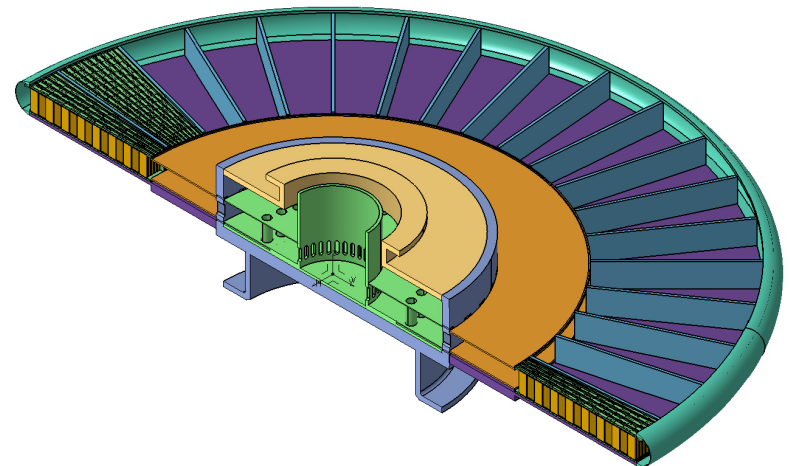
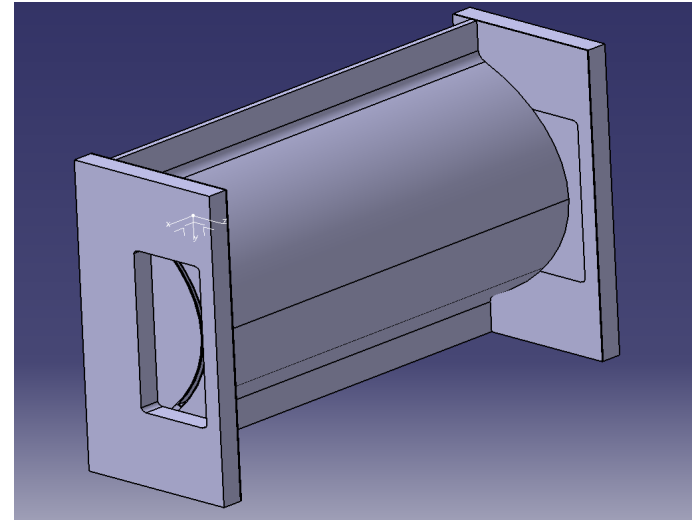


Halo monitoring and δ -ray

- Δ -ray introduces negative charge deposition in the aperture monitor intersecting halo
 - During normal operation, the aperture monitor expects to produce noise signal.
 - In case of beam offset, more protons will be intersected by nickel diaphragms, producing “positive net charge deposition.”

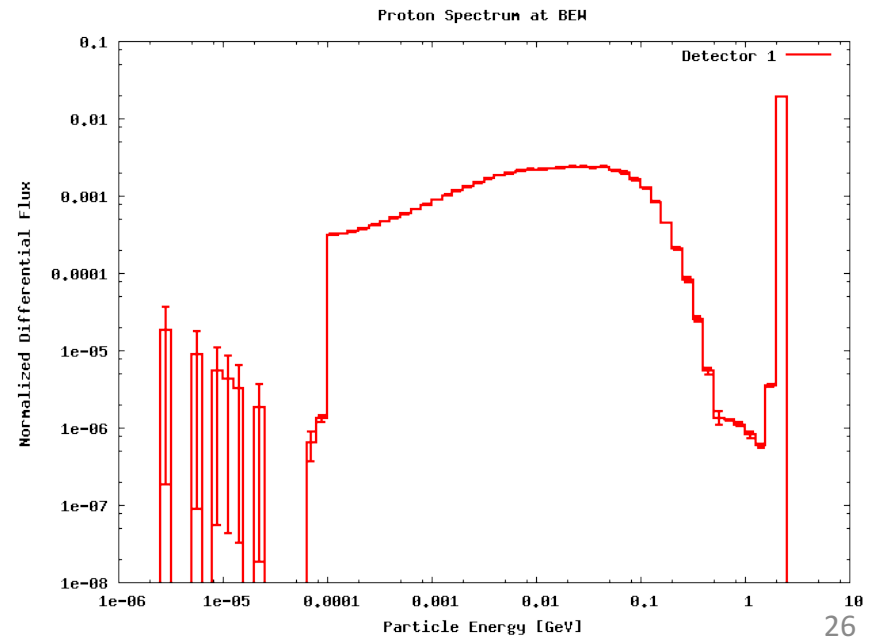
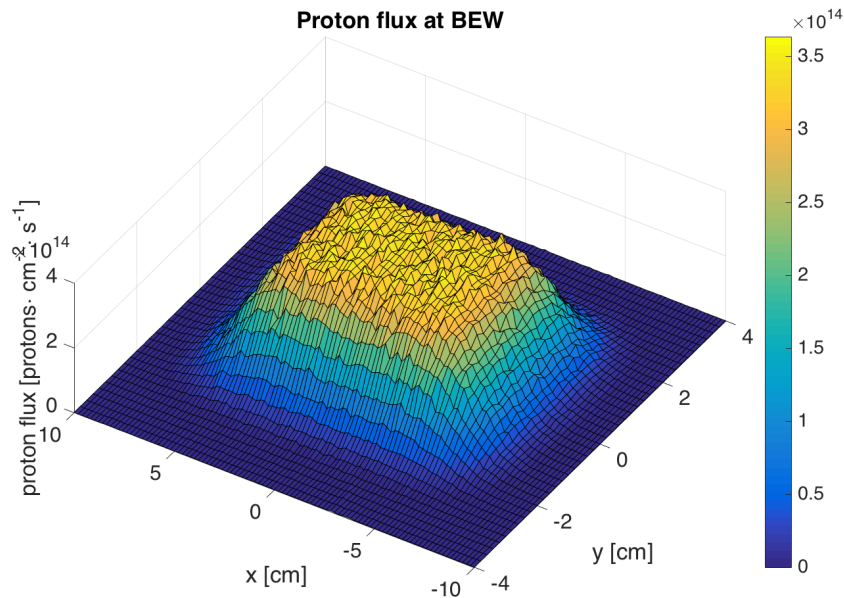
Luminescent coating

- Luminescent coatings on PBW and target for the beam profile imaging
- Baseline material:
 - Benchmarking SNS
 - Cr (1%) doped alumina (Al_2O_3)

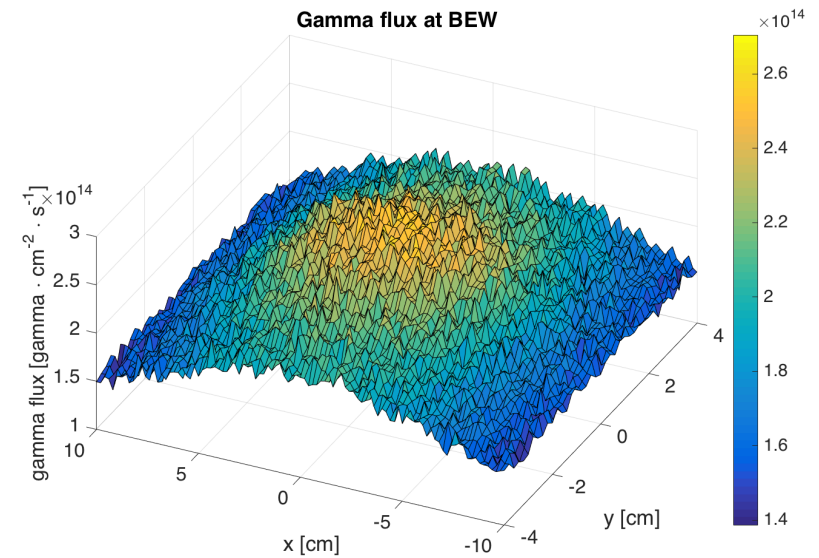
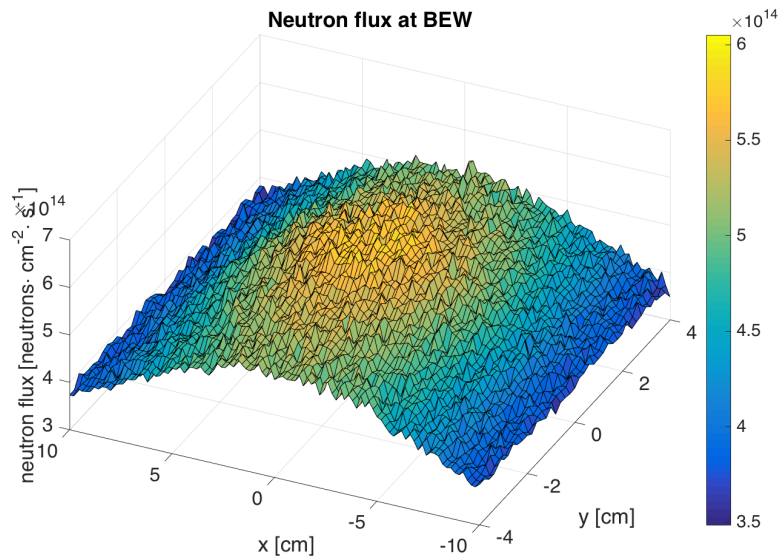
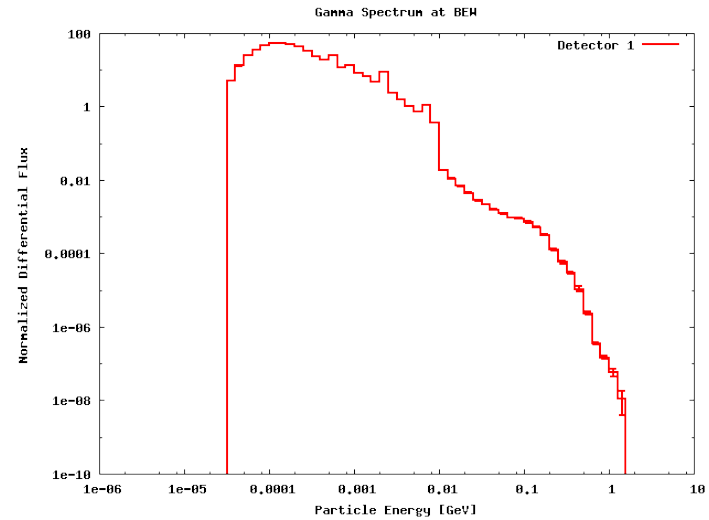
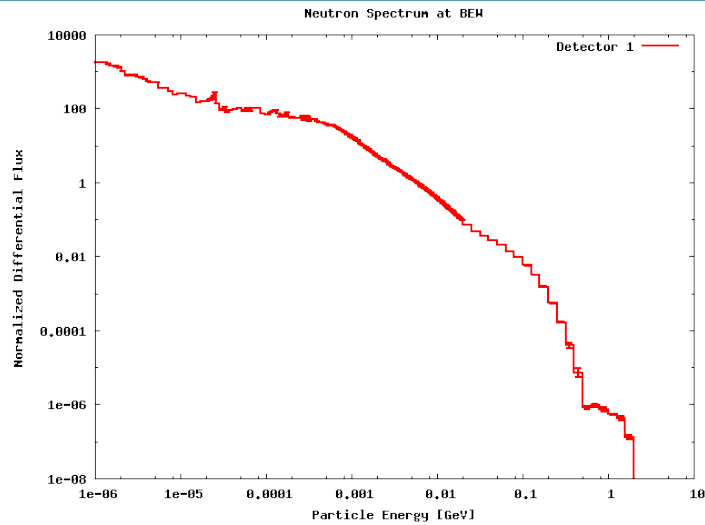


Proton flux at BEW

- Secondary protons from the harp



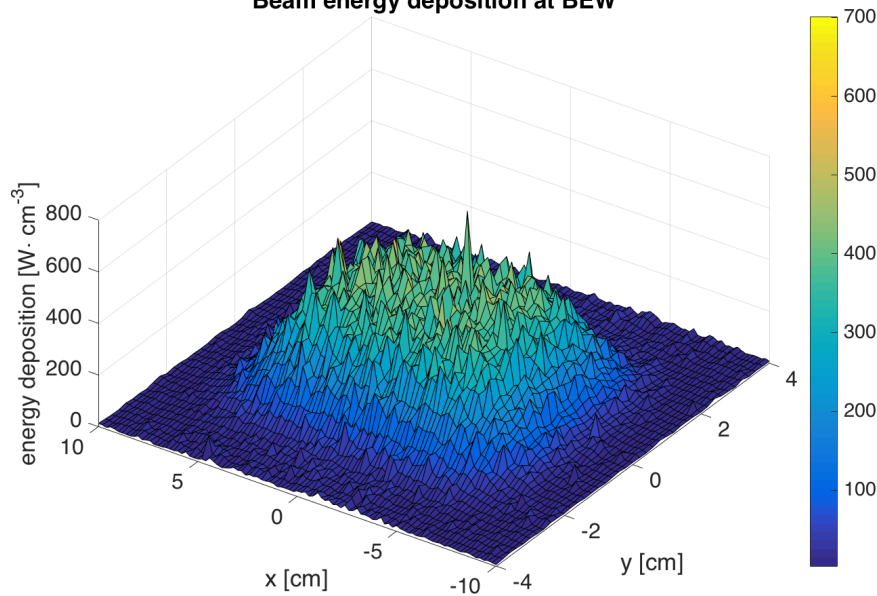
Neutron and gamma flux at BEW



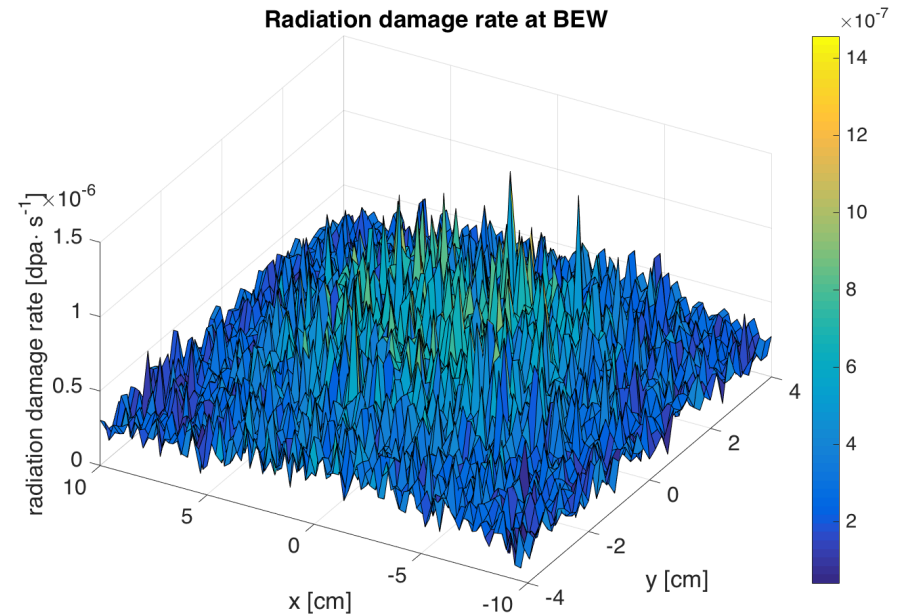
Energy deposition and radiation damage at BEW

- The radiation damage doesn't follow the proton beam profile

Beam energy deposition at BEW



Radiation damage rate at BEW



Issues in luminescent coating

- Radiation induced luminosity degradation

- Excit
 - Etc.
- Thomas Shea et al., "Luminescent materials development for beam-on-target imaging at the European Spallation Source."***

- The SiC is chosen to be the baseline material for the harp
- The Ni-diaphragm for halo monitoring will generate noises during normal beam operation, due to δ -rays from the harp and upstream components. But, it should be able to detect the anomalous beam position offset.
- There is on-going research on the luminescent coating material. Currently, baseline material is Cr:Al₂O₃ as at SNS.

Thank you!

